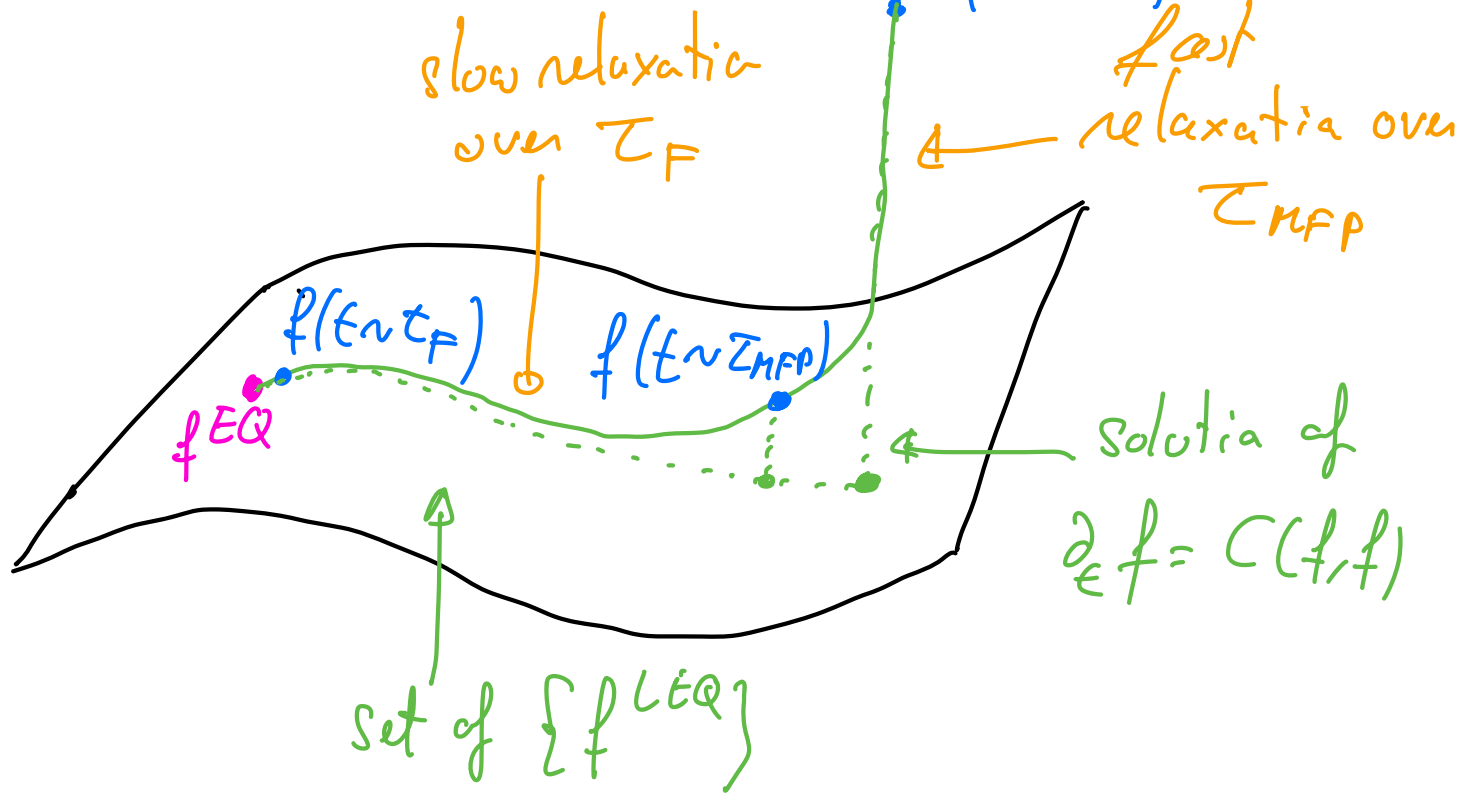


(1)



Perturbation theory

$$f(\vec{q}, \vec{p}, t) = f_0(\vec{q}, \vec{p}, t) + \epsilon f_1(\vec{q}, \vec{p}, t)$$

Hydrodynamic fields

$$\int f d\rho = n(q)$$

$$\int \vec{v} f d\rho = n(\vec{q}) \vec{u}(\vec{q}) : \vec{v} = \frac{\vec{p}}{m}$$

$$\int \frac{m}{2} (\vec{v} - \vec{u})^2 f d\rho = n(\vec{q}) \varepsilon(\vec{q}) = \frac{3}{2} n(\vec{q}) h_B T(\vec{q})$$

leading order (BE)

$$\hat{C}(f, f) = 0 \Rightarrow f_0(\vec{q}, \vec{p}, t) = \frac{n}{(2\pi m h_B T)^{3/2}} e^{-\frac{m \delta \vec{v}^2}{2 h_B T}}$$

$$\delta \vec{v}(\vec{q}, \vec{p}, t) = \vec{v} - \vec{u}(\vec{q}, t)$$

Hydrodynamic equations

(2)

$$D_t m \equiv (\partial_t + u_\alpha \partial_{q_\alpha}) m = -m \partial_{q_\alpha} u_\alpha$$

$$M D_t u_\alpha = -\frac{1}{m} \partial_{q_\beta} \cdot P_{\alpha\beta} \Leftrightarrow M D_t \vec{u} = -\frac{1}{m} \vec{\nabla} \cdot \vec{P}$$

with $P_{\alpha\beta} = m m \langle \delta v_\alpha \delta v_\beta \rangle$

$$\partial_t T + u_\alpha \partial_\alpha T = -\frac{2}{3m h_\beta} \partial_\alpha h_\alpha - \frac{2}{3m h_\beta} P_{\alpha\beta} u_{\alpha\beta}$$

where

- $u_{\alpha\beta} = \frac{1}{2} (\partial_{q_\alpha} u_\beta + \partial_{q_\beta} u_\alpha)$ is the *strain rate tensor*
- $h_\alpha = \frac{m M}{2} \langle \delta v_\alpha \delta v_\beta \delta v_\beta \rangle$ is the *heat flux*

Closure: To compute the evolution of $m, T, \vec{u}$, we need to compute $P_{\alpha\beta} = m m \langle \delta v_\alpha \delta v_\beta \rangle$ & $h_\alpha = \frac{m M}{2} \langle \delta v_\alpha \delta v_\beta \delta v_\beta \rangle$, which we can do perturbatively using f :

$$m, T, \vec{u} \Rightarrow f_0 \Rightarrow P_{\alpha\beta}^0, h_\alpha^0 \Rightarrow \partial_t (m, T, \vec{u})^0 \Rightarrow \partial_t f_0$$

Pressure & heat flux

$$P_{\alpha\beta}^0 = m m \langle \delta v_\alpha \delta v_\beta \rangle_0 = m k_B T \delta_{\alpha\beta} \quad \text{ideal gas law}$$

$u_x^0 = 0$ because it involves an odd moment of δv

Leading order dynamics

$$\partial_\epsilon m + u_\alpha \partial_{q_\alpha} m = -m \partial_{q_\alpha} u_\alpha \quad (1)$$

$$M \partial_\epsilon u_\alpha + M u_\beta \partial_{q_\beta} u_\alpha = -\frac{1}{m} \partial_{q_\alpha} [m u T] \quad (2)$$

$$\partial_\epsilon T + u_\alpha \partial_{q_\alpha} T = -\frac{2}{3} T \partial_{q_\alpha} u_\alpha \quad (3)$$

Q: Do these equations lead f_0 to f^{Eq} ?

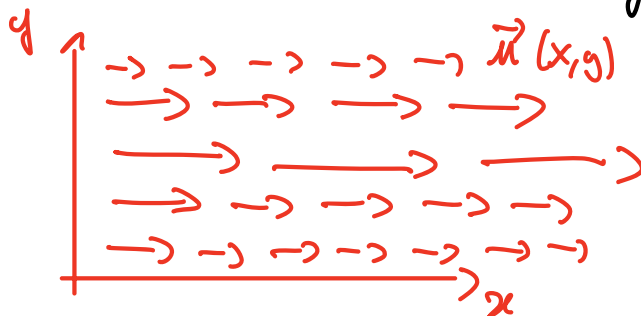
No relaxation of shear modes

let us consider an initial condition in which the gas is sheared:

$$n_0 = \bar{n} \text{ uniform}$$

$$T_0 = \bar{T} \text{ uniform}$$

$$\vec{u} = u(y) \vec{e}_x$$



$$\text{In eq (1); } \vec{\nabla} \cdot (m_0 \vec{T}_0) = 0 \quad \& \quad \vec{u} \cdot \vec{\nabla} \vec{u} = u(y) \partial_x u(y) \vec{e}_x = 0$$

$$\Rightarrow \partial_\epsilon \vec{u}_0 = 0 \quad \& \quad \vec{u}_0 \text{ is NOT relaxing to } \vec{u} = 0 \dots$$

At order ϵ^0 , f^{LEQ} does not necessarily relax to $f^{\text{Eq}} \Rightarrow$ high order!

2.4.4) First-order hydrodynamics

4

Single time approximation: $\partial_\epsilon f = C(f, f)$ makes f relax to f_0 in a time $\sim \tau_{MFP}$, thanks to a complicated superposition of processes involving time scales spanning $[\tau_{col}, \tau_{MFP}]$.

Seen from a larger time, we approximate this as a **single**

relaxation process: $\partial_\epsilon f \simeq -\frac{1}{\tau_{MFP}} (f - f_0)$

$$\Rightarrow C(f, f) \simeq -\frac{1}{\tau_{MFP}} (f - f_0) = -\frac{1}{\tau_{MFP}} (\epsilon f_1 + \epsilon^2 f_2 + \dots) \quad \text{when } \epsilon = \frac{\tau_{MFP}}{\tau_F}$$
$$\simeq -\frac{1}{\tau_F} f_1$$

Rescaled dynamics $t = \tau_F \hat{t}$

$$\partial_{\hat{t}} f = -L_F f + \frac{1}{\epsilon} \hat{C}(f, f) \quad \text{with} \quad \hat{C}(f, f) = \tau_{MFP} C(f, f)$$
$$\simeq -\epsilon f_1$$

$$\Rightarrow \partial_{\hat{t}} f = -L_F f - f_1 \quad ; \quad f = f_0 + \epsilon f_1$$

$$\Rightarrow \mathcal{O}(\epsilon^0): \quad \partial_{\hat{t}} f_0 = -L_F f_0 - f_1$$

$$\Rightarrow f_1 = -L_F f_0 - \partial_{\hat{t}} f_0 = -\tau_F \left(\vec{v} \cdot \partial_{\vec{q}} f_0 + \partial_{\hat{t}} f_0 \right)$$

known from leading order hydro

easier than working with $\hat{t}$ to use hydrodynamic equations

(5)

Finally, we write $f = f_0 + \varepsilon f_1 = f_0 (1 + g_1)$

with $g_1 = -\tau_{\text{HFP}} \left(\partial_t \ln f_0 + \vec{v} \cdot \partial_{\vec{q}} \ln f_0 \right)$ that we need to determine to leading order in $\varepsilon \Rightarrow$ use 0th order hydrodynamics for the right-hand side.

Logic:

$$O\left(\frac{1}{\varepsilon}\right) \Rightarrow f_0 \Rightarrow h, p_{\alpha\beta}^0 \Rightarrow n_0, T_0, \mu_0 \stackrel{O(1)}{\Rightarrow} f_1 \Rightarrow h, p_{\alpha\beta}^1 \Rightarrow n_1, T_1, \mu_1$$

First order phase-space density:

Using $f_0 = \frac{n_0}{(2\pi m k_B T_0)^{3/2}} e^{-\frac{m \delta \vec{v}^2}{2 k_B T_0}}$ leads to

$$g_1 = -\tau_{\text{HFP}} \left(\partial_t + v_\alpha \partial_{q_\alpha} \right) \left[\ln n_0 - \frac{3}{2} \ln T_0 - \frac{m \delta \vec{v}^2}{2 k_B T_0} \right]$$

Using $D_t n_0 = -n_0 \partial_{q_\alpha} \mu_\alpha^0$

$$m D_t \mu_\alpha^0 = -\frac{1}{n_0} \partial_{q_\alpha} [n_0 k_B T_0]$$

$$D_t T_0 = -\frac{2}{3} T_0 \partial_{q_\alpha} \mu_\alpha^0$$

leads to

$$g_1 = -\frac{\tau_{\text{HFP}} m}{k_B T_0} \mu_{\alpha\beta}^0 \left(\delta v_\alpha \delta v_\beta - \frac{\delta \vec{v}^2}{3} \delta_{\alpha\beta} \right) - \frac{\tau_{\text{HFP}}}{T_0} \left(\partial_{q_\alpha} T_0 \right) \left(\frac{m \delta \vec{v}^2}{2 k_B T_0} - \frac{5}{2} \right)$$

Note that $g_1(\bar{T}_0, v^0) = g_1(\bar{T}, v) + O(\varepsilon) \Rightarrow$ correct equivalent to this order

(6)

Proof: Drop the "0" sub & superscript & use

$$\partial_\epsilon + v_\alpha \partial q_\alpha = D_\epsilon + (v_\alpha - u_\alpha) \partial_\alpha = D_\epsilon + \delta v_\alpha \partial q_\alpha$$

$$-\frac{g_1}{T_{HFP}} = \frac{1}{n} (D_\epsilon + \delta v_\alpha \partial q_\alpha) n - \frac{3}{2T} (D_\epsilon + \delta v_\alpha \partial q_\alpha) T - \frac{m}{2h_B} (D_\epsilon + \delta v_\alpha \partial q_\alpha) \frac{\delta \vec{v}^2}{T}$$

$$= \textcircled{1}: \underbrace{-\partial q_\alpha u_\alpha - \frac{3}{2} \left(-\frac{1}{3} \partial q_\alpha u_\alpha \right)}_{=0} - \frac{m}{2h_B} \cancel{2} \delta v_\beta \frac{D_\epsilon (-u_\beta)}{T} + \frac{m}{2h_B} \frac{\delta \vec{v}^2}{T^2} D_\epsilon T$$

$$\textcircled{2} + \frac{\delta v_\alpha}{n} \partial q_\alpha n - \frac{3 \delta v_\alpha}{2T} \partial q_\alpha T - \frac{m \delta v_\alpha}{2h_B} \left(\frac{2 \delta v_\beta}{T} \partial q_\alpha (-u_\beta) - \frac{\delta \vec{v}^2}{T^2} \partial q_\alpha T \right)$$

$$= \frac{m}{h_B T} \delta v_\beta \left(-\frac{1}{n n} \partial q_\beta (n h_B T) \right) - \frac{m}{2h_B} \frac{\delta \vec{v}^2}{T^2} \frac{2}{3} T \partial q_\alpha u_\alpha$$

$$+ \frac{\delta v_\alpha}{n} \partial q_\alpha n - \frac{\delta v_\alpha}{T} \partial q_\alpha T \left(\frac{3}{2} - \frac{m \delta \vec{v}^2}{2 h_B T} \right) + \frac{m}{h_B T} \underbrace{\delta v_\alpha \delta v_\beta \partial q_\alpha u_\beta}_{= \delta v_\alpha \delta v_\beta u_{\alpha\beta}}$$

$$= -\frac{\delta v_\beta}{T} \partial q_\beta T - \frac{m}{3 h_B T} \underbrace{\delta \vec{v}^2 \partial q_\alpha u_\alpha}_{u_{\alpha\beta} \delta \alpha\beta} - \frac{\delta v_\alpha}{T} \partial q_\alpha T \left(\frac{3}{2} - \frac{m}{2} \frac{\delta \vec{v}^2}{h_B T} \right) + \frac{m}{h_B T} \delta v_\alpha \delta v_\beta u_{\alpha\beta}$$

$$g_1 = -T_{HFP} \frac{m}{h_B T} u_{\alpha\beta} \left[\delta v_\alpha \delta v_\beta - \frac{\delta \vec{v}^2}{3} \delta_{\alpha\beta} \right] + T_{HFP} \frac{\delta v_\alpha}{T} \partial q_\alpha T \left(\frac{5}{2} - \frac{m \delta \vec{v}^2}{2 h_B T} \right)$$

First order pressure & heat flux:

$$f = f_0 (1 + g_1) \Rightarrow \langle O \rangle_f = \langle O (1 + g_1) \rangle_{f_0}$$

$$\Rightarrow p_{\alpha\beta} = n n \langle \delta v_\alpha \delta v_\beta \rangle = n n \langle \delta v_\alpha \delta v_\beta \rangle_0 - n n^2 \frac{T_{HFP}}{h_B T} u_{\gamma\delta} \left[\right.$$

$$\left. \langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\delta \rangle - \frac{\delta \gamma \delta}{3} \langle \delta v_\alpha \delta v_\beta \delta \vec{v}^2 \rangle \right] + 0$$

$\uparrow$
 $\langle \delta \vec{v} \dots \delta \vec{v} \rangle$
 odd # of $\delta \vec{v}$

Wick theorem

(7)

Moments of Gaussians are given by the sum over all possible unitary pairings.

$$\langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\delta \rangle_0 = \frac{(\hbar_B T)^2}{m^2} \left(\delta_{\alpha\beta} \delta_{\gamma\delta} + \delta_{\alpha\gamma} \delta_{\beta\delta} + \delta_{\alpha\delta} \delta_{\beta\gamma} \right)$$

$$\Rightarrow \mu_{\gamma\delta} \langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\delta \rangle = \frac{(\hbar_B T)^2}{m^2} \left(\mu_{\gamma\gamma} \delta_{\alpha\beta} + 2 \mu_{\alpha\beta} \right)$$

$$\langle \delta v_\alpha \delta v_\beta \delta v_\gamma \delta v_\gamma \rangle = \frac{(\hbar_B T)^2}{m^2} \left(3 \delta_{\alpha\beta} + 2 \underbrace{\delta_{\alpha\gamma} \delta_{\beta\gamma}}_{\delta_{\alpha\beta}} \right) = 5 \delta_{\alpha\beta} \frac{(\hbar_B T)^2}{m^2}$$

$$\Rightarrow P_{\alpha\beta} = m \hbar_B T \delta_{\alpha\beta} - m \hbar_B T \tau_{\text{HFP}} \left(2 \mu_{\alpha\beta} + \mu_{\gamma\gamma} \delta_{\alpha\beta} - \frac{5}{3} \mu_{\gamma\gamma} \delta_{\alpha\beta} \right)$$

$$P_{\alpha\beta} = m \hbar_B T \left[\delta_{\alpha\beta} \left(1 + \frac{2}{3} \tau_{\text{HFP}} \mu_{\gamma\gamma} \right) - 2 \tau_{\text{HFP}} \mu_{\alpha\beta} \right]$$

Relaxation of shear flow: $\vec{u} = u(y) \vec{e}_x$

$$\mu_{\alpha\beta} = \frac{1}{2} \left(\partial_\alpha u_\beta + \partial_\beta u_\alpha \right) = \frac{1}{2} \left(\delta_{\alpha y} \delta_{\beta x} + \delta_{\beta y} \delta_{\alpha x} \right) u'(y)$$

$$P_{\alpha\beta} = m \hbar_B T \delta_{\alpha\beta} - m \hbar_B T \tau_{\text{HFP}} \left(\delta_{\alpha y} \delta_{\beta x} + \delta_{\beta y} \delta_{\alpha x} \right) u'(y)$$

$$m D_\epsilon u_x = - \frac{1}{m} \partial_{q_x} P_{\alpha x}$$

$$\Leftrightarrow m D_\epsilon u(y) + m u_x \cdot \underbrace{\partial_x u(y)}_{=0} + m u_y \cdot \underbrace{\partial_y u(y)}_{=0} = - \frac{1}{m} \partial_y \left(- m \hbar_B T \tau_{\text{HFP}} u'(y) \right)$$

$$\text{For } \frac{m}{T} = n_0 \Rightarrow \partial_\epsilon u(y, \epsilon) = \underbrace{\frac{\tau_{\text{HFP}} \hbar_B T}{m}}_{\eta \text{ is the kinematic viscosity}} \partial_{yy} u(y, \epsilon) \quad \text{diffusion equation}$$

8

- (i) f_1 alters the statistics of f , and thus ρ_{eq} & h_{eq}
- (ii) Transport makes the hydrodynamic field relax



where κ is the thermal conductivity $\kappa = \frac{5}{2} \frac{m \hbar_B^2 T}{m} T_{HFP}$

$$x h_a = \frac{n n}{2} \langle \delta v_a \delta \vec{v}^2 (1+g_1) \rangle_0 \rightarrow \text{only even powers matter}$$

$\xrightarrow{\text{odd}} \text{in } g_1$

* We need to compute $\langle \delta v_o \delta v_r \delta v_e \delta v_f \delta v_a \delta v_b \rangle = \frac{h^3 T^3}{h^3} \delta_{\alpha\beta} \times (\text{combinatorial factor})$

All possible pairings (1) Graph strategy

$$\left. \begin{array}{l} \delta \bigcirc \delta \rightarrow \delta_{\delta\delta} = 3 \\ \text{---} \bullet \text{---} \rightarrow \delta_{\alpha\beta} \\ \varepsilon \bigcirc \varepsilon \rightarrow \delta_{\varepsilon\varepsilon} = 3 \end{array} \right\} 9 \delta_{\alpha\beta}$$

$$\left. \begin{array}{l} \alpha \text{---} \bullet \text{---} \varepsilon \text{---} \bullet \text{---} \varepsilon \text{---} \bullet \text{---} \beta \\ \delta \bigcirc \delta \rightarrow \times 3 \end{array} \right\} 6 \delta_{\alpha\beta}$$

$$\left. \begin{array}{l} \alpha \text{---} \bullet \text{---} \delta \text{---} \bullet \text{---} \delta \text{---} \bullet \text{---} \beta \\ \varepsilon \bigcirc \varepsilon \rightarrow 3 \end{array} \right\} 6 \delta_{\alpha\beta}$$

$$\left. \begin{array}{l} \alpha \text{---} \bullet \text{---} \beta \quad \delta_{\alpha\beta} \\ \varepsilon \text{---} \bullet \text{---} \delta \text{---} \bullet \text{---} \varepsilon \quad \times 2 \delta_{\varepsilon\varepsilon} = 6 \end{array} \right\} 6 \delta_{\alpha\beta}$$

$$\alpha \text{---} \bullet \text{---} \varepsilon \text{---} \bullet \text{---} \varepsilon \text{---} \bullet \text{---} \delta \text{---} \bullet \text{---} \delta \text{---} \bullet \text{---} \beta \quad 4 \delta_{\alpha\beta}$$

$$\alpha \text{---} \bullet \text{---} \delta \text{---} \bullet \text{---} \delta \text{---} \bullet \text{---} \varepsilon \text{---} \bullet \text{---} \varepsilon \text{---} \bullet \text{---} \beta \quad 4 \delta_{\alpha\beta}$$

$$\Rightarrow 35 \delta_{\alpha\beta}$$

(2) Math strategy. Sum only if $\sum_i$ explicit.

$$\sum_{\varepsilon, \delta} \langle \delta v_\alpha \delta v_\beta \delta v_\varepsilon \delta v_\varepsilon \delta v_\delta \delta v_\delta \rangle = \delta_{\alpha\beta} \langle \delta v_\alpha^2 \sum_\varepsilon \delta v_\varepsilon^2 \sum_\delta \delta v_\delta^2 \rangle$$

$$= \delta_{\alpha\beta} \left[\langle \delta v_\alpha^6 \rangle_{\varepsilon=\delta=\alpha} + 2 \sum_{\varepsilon \neq \alpha} \langle \delta v_\alpha^4 \delta v_\varepsilon^2 \rangle_{\delta=\alpha} \right]$$

$$+ \sum_{\varepsilon \neq \alpha} \langle \delta v_\alpha^2 \delta v_\varepsilon^4 \rangle + \sum_{\varepsilon \neq \delta \neq \alpha} \langle \delta v_\alpha^2 \delta v_\varepsilon^2 \delta v_\delta^2 \rangle$$

$$= \delta_{\alpha\beta} \left[5 \langle \delta v_\alpha^2 \rangle \langle \delta v_\alpha^4 \rangle + 4 \langle \delta v_\alpha^4 \rangle \langle \delta v_\varepsilon^2 \rangle \right]$$

$$+ 2 \langle \delta v_\alpha^2 \rangle \langle \delta v_\varepsilon^4 \rangle + 2 \langle \delta v_\alpha^2 \rangle \langle \delta v_\varepsilon^2 \rangle \langle \delta v_\delta^2 \rangle$$

$$= \delta_{\alpha\beta} \left[15 \left(\frac{\hbar \beta T}{m} \right)^3 + 12 \left(\frac{\hbar \beta T}{m} \right)^3 + 6 \left(\frac{\hbar \beta T}{m} \right)^3 + 2 \left(\frac{\hbar \beta T}{m} \right)^3 \right]$$

$$= 35 \left(\frac{\hbar \beta T}{m} \right)^3 \delta_{\alpha\beta}$$

$$h_\alpha = -\frac{m H \tau_{\text{MFP}}}{2T} (\partial_{q_\beta} T) \left\langle \frac{M}{2hT} (\delta \vec{v})^2 \delta v_\beta \delta v_\alpha - \frac{5}{2} \delta \vec{v}^2 \delta v_\alpha \delta v_\beta \right\rangle$$

$$= -\frac{m H \tau_{\text{MFP}}}{4T} (\partial_{q_\beta} T) \delta_{\alpha\beta} \left(\frac{M}{hT} \cdot 35 \left(\frac{h_\beta T}{M} \right)^3 - 25 \left(\frac{h_\beta T}{M} \right)^2 \right)$$

$$h_\alpha = -\frac{5}{2} \frac{m}{M} \tau_{\text{MFP}} h_\beta^2 T (\partial_{q_\alpha} T)$$

First-order hydrodynamics

$$D_\epsilon m = -m \partial_{q_\alpha} u_\alpha$$

$$m D_\epsilon u_\alpha = -\frac{1}{m} \partial_{q_\beta} \cdot P_{\alpha\beta} = -\frac{1}{m} \partial_{q_\alpha} \left[m h_\beta T + \frac{2}{3} m h_\beta T \tau_{\text{MFP}} \partial_r v_r \right] \\ + \frac{1}{m} \partial_{q_\beta} \left[m h_\beta T \tau_{\text{MFP}} u_{\alpha\beta} \right]$$

$$D_\epsilon T = \frac{5}{3 m h_\beta} \partial_{q_\alpha} \left[\frac{m}{m} \tau_{\text{MFP}} h_\beta^2 T \partial_{q_\alpha} T \right] - \frac{2T}{3} \left[\partial_{q_\alpha} u_\alpha - \tau_{\text{MFP}} u_{\alpha\beta} u_{\alpha\beta} + \frac{2}{3} \tau_{\text{MFP}} (\partial_\alpha v_\alpha)^2 \right]$$

Relaxation to equilibrium

$$m = m_0 + \delta m; \quad \vec{u}' = \delta \vec{u}'; \quad T = T_0 + \delta T$$

$$\text{linearized dynamics for } \begin{pmatrix} \delta m \\ \delta \vec{u}' \\ \delta T \end{pmatrix}: \quad \partial_\epsilon \begin{pmatrix} \delta m \\ \delta \vec{u}' \\ \delta T \end{pmatrix} = M \cdot \begin{pmatrix} \delta m \\ \delta \vec{u}' \\ \delta T \end{pmatrix}$$

The eigenvalues of M have negative real parts, leading to the

decay of the perturbation & the convergence to equilibrium ($\vec{u}'=0$, $T=T_0$ & $m=m_0$).

Few more thoughts

(11)

We set up a nice perturbation for f & then come back to ϵ when computing hydrodynamic equations, which is frustrating.

A longer but neater route consist in rescaling also the hydrodynamic time & mods.

$$\text{To } t = \hat{t} \tau_F \text{ correspond } \boxed{\vec{p} = \frac{1}{\tau_F} \hat{\vec{p}}}$$

$$\hat{m} = m \text{ s.t. that } \hat{f} d\hat{\vec{p}} = f d\vec{p} \text{ \& } \boxed{f = \tau_F \hat{f}}.$$

$$\vec{u} = \int d\vec{p} f \vec{p} = \frac{1}{\tau_F} \int d\hat{\vec{p}} \hat{f} \hat{\vec{p}} \Rightarrow \boxed{\vec{u} = \frac{1}{\tau_F} \hat{\vec{u}}}$$

$$\text{Similarly, } \boxed{T = \frac{1}{\tau_F} \hat{T}, \quad D_t = \frac{1}{\tau_F} \hat{D}_t, \quad P_{\alpha\beta} = \frac{1}{\tau_F^2} \hat{P}_{\alpha\beta}, \quad h_\alpha = \frac{1}{\tau_F^3} \hat{h}_\alpha}$$

All this follows from algebra, but also simply from dimensional analysis.

The hydrodynamic equations read

$$\partial_t m = -\partial_{\vec{q}} \cdot [\hat{\vec{u}} m]; \quad m \hat{D}_t \hat{\vec{u}} = -\frac{1}{\hat{m}} \partial_{\vec{q}} \cdot \hat{\vec{p}}; \quad \hat{D}_t \hat{T} = -\frac{2}{3\hat{m}h_B} \partial_{\vec{q}} \cdot \hat{\vec{h}} - \frac{2}{3\hat{m}h_B} \hat{\nabla} \otimes \hat{\vec{u}} : \hat{P}$$

The *zeroth order* hydro then follows as before & $\hat{f}_0 = \frac{\hat{m}_0}{(2\pi m h_B \hat{T}_0)^{3/2}} e^{-\frac{\delta \vec{v}^2}{2 h_B \hat{T}_0}}$

$$\text{leading to } \partial_t \vec{u} = -\hat{\nabla} \cdot [\hat{\vec{u}} m]$$

$$m \hat{D}_t \vec{u} = -\frac{1}{m} \hat{\nabla} \cdot [m h_B \hat{T}] \Rightarrow \text{no relaxation}$$

$$\hat{D}_t \hat{T} = -\frac{2\hat{T}}{3} \hat{\nabla} \cdot \hat{\vec{u}}$$

The first order now takes a nicer form